ALBERTA TRANSPORTATION AND ECONOMIC CORRIDORS GRMP NORTH CENTRAL (ATHABASCA AND FORT McMURRAY DISTRICTS) 2024 SITE INSPECTION



Site Number	Location		Name				Hwy	km		
NC097 Fort McMu		urray		Parsons Road Overpass/Hwy 63			wy	686:20		
Legal Description			UTM Co-ordinates (NAD 83)			33)				
SW7-90-9-W4 12V N 6,293,600 E 473,700									0	
			Date		PF	CF	Total		al	
Previous Inspection:		May 18, 2023			11	4	44 (Landslide basis)		de basis)	
Current Inspection:		June 5, 2024			11	5	55 (Landslide basis)		de basis)	
Road WAADT:		4,78		0		Year:	2023		3	
Inspected By:		José Pineda, Tarek Abdelaziz (Thurber) Rocky Wang (TEC)								
Report Attachments:		Photograph			ns 🔽 Plans			C Maintenance Items		
Primary Site Issue:			A crack formed across both traffic directions along the top of the Parsons Road overpass (BF85178), ~6 m west of the west abutment (along the western edge of the approach slab); settlement of west approach slab causing a dip behind the west abutment (possibly due to bridge west headslope movement).							
Dimensions:			The cracks are across eastbound and westbound lanes (26 m long), dip is within the boundaries of the approach slab (26 m wide x 6 m long).							
Site History:			Based on information provided by TEC and an examination of the as- built drawings, weak soil overlying limestone bedrock existed at this overpass location. An instrumented test fill was built at the east headslope, supported on a wick drain perforated foundation soil. Based on the performance of that test fill it was determined that in order to meet the construction schedule demands the weak soils had to be completely excavated from the west headslope area (up to 7 m in depth), and the portion of the east headslope not covered by the instrumented test fill (up to 5 m in depth). Engineered fill, mainly consisting of clay shale, was placed to restore the grades, and then the headslope fills were constructed overtop original grade level (up to 13 m in height). The west headslope fill was built with geogrid reinforcement clay shale. An extensive instrumentation program consisting of slope inclinometers, piezometers and settlement cells were installed to monitor construction activities, control fill placement rates, and provide post construction information. Thurber is currently monitoring these instruments as part of the GRMP geohazards contract.							
Maintenance:		ACP Patch was placed in 2020 and 2022 on eastbound and westbound lanes. Between 2023 and 2024: Milled and patched the highway within the impacted area, placed a flexible filler to seal the gaps between the wing walls and the drain troughs, filled the void under the abutment seat with grout.								

Observations:	Description	Worse?
Pavement Distress	Up to 60 mm wide x 90 mm deep x 26 m long crack reflected through the patch along the western edge of the west approach slab, about 6 m west of the west abutment; previously noted dip on the eastbound and westbound lanes west of the Finger Plate Joint were not visible in the 2024 site inspection.	
Slope Movement	Bridge head slope was noted to have moved laterally and vertically by up to 300 in 2023. In 2024, additional movements of about 10 mm (lateral) and about 20 mm (vertical) were noted.	2
Erosion	Rutting at the toe of the headslope	2
Seepage	Ponding water at the toe of the headslope	
Bridge/Culvert Distress	200 to 300 mm of head slope movement; no visible cracks on abutment walls, wing walls, and abutment slope concrete facing; bridge bearing plates movement maxed out	2
C Other		

Instrumentation: (6 SIs, 28 VWs, 4SCs)

The following is a summary of the readings of the closest instruments to the bridge west headslope (between spring 2023 and spring of 2024):

SI14-05 located at the toe of the headslope is moving at 7.7 mm/yr over 1.5 and 4.6 m depth and at 0.5 mm/yr over 4.6 m to 9.4 m; The total lateral movement recorded in SI14-05 since 2014 is 102 mm; the increases in settlement values since the spring of 2023 in operational settlement cells are: SC14-09= 25 mm, SC14-12=22 mm, SC15-04= 11mm, and SC15-06= 7 mm.

Assessment (Refer to attached Figure):

The site observations and instrumentation monitoring results indicate "excessive" vertical and lateral movements of the west approach fill. The cracks and the dips noted on the driving lanes are reflections of the ongoing slope movement of the approach fill. The movement of the fill appears to have created voids below the approach slab.

The repair work completed by TEC between 2023 and 2024 improved the situation temporarily. The voids below the approach slab and the abutment seat will likely get bigger in size and additional movement of the head slope may impact the integrity of the highway and the bridge. Furthermore, surface water infiltration into open cracks on the road will likely saturate and soften the high plastic approach fill, and may result in an accelerated slope movement.

The Consequence Factor was increased from 4 to 5 since either a significant detour and/or road closure may have to take place in response to an accelerated slope movement.

The accumulated water at the bottom of the west headslope is likely a reflection of poor surface drainage in this area. The toe is also bare of vegetation and the water accumulating at the toe has created a soft zone with multiple rutting as a result of off terrain vehicle traffic in this area.

Recommendations:

It is recommended to visit the site again in 2025.

It is recommended to install at least two slope inclinometers at this site (one at the top of the slope and another one at the bottom of the slope) to assess the potential depth and the extent of headslope

movement. Consideration should also be given to installing extensometers/settlement cells within the severely impacted areas of the approach fill to fully characterize the bridge headslope movement.

A structural engineer should be consulted in the near future to (a) examine the condition of the bridge and assess whether the structure is performing as per the original design, and (b) provide recommendations for rehabilitation/repairs (if needed) and instrumentation monitoring of structural elements (if required).

Short Term:

The local MCI should periodically monitor existing cracks and dips (if developed on the highway surface due to excessive movement). The bridge abutment walls and seat; and bridge approach fill slopes should also be monitored for any signs of additional movements.

The cracks on the highway should be sealed, and ACP patch should also be placed if a significant dip occurs on the highway surface. As recommended in the past it is ideal to drill holes within the slab to and inject grout in the holes to fill any voids below the slab. This may lessen the frequency of milling and patching on the highway.

Existing and future gaps (if developed) under drain troughs, between drain troughs and wingwalls, and below the abutment seat under the bridge should be filled with low strength fillcrete.

The ground surface at the toe the headslope should be slightly regraded to avoid ponding of water and the re-graded surface should be topsoiled, seeded, and covered with a heavy-duty erosion control product.

Medium to Long Term:

Preliminary engineering is recommended to assess the cause of the observed movements and provide potential remedial measures and associated "A" estimates. New geotechnical instrumentation should be installed and monitored to complete this assessment.

Closure

It is a condition of this letter report that Thurber's performance of its professional services will be subject to the attached Statement of Limitations and Conditions.

Tarek Abdelaziz, Ph.D., P.Eng. Partner | Senior Geotechnical Engineer

José Pineda, M.Eng., P.Eng. Associate | Senior Geotechnical Engineer



STATEMENT OF LIMITATIONS AND CONDITIONS

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This Report has been prepared in accordance with generally accepted engineering or environmental consulting practices in the applicable jurisdiction. No other warranty, expressed or implied, is intended or made.

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The Report has been prepared for the specific site, development, design objectives and purposes that were described to Thurber by the Client. The applicability and reliability of any of the findings, recommendations, suggestions, or opinions expressed in the Report, subject to the limitations provided herein, are only valid to the extent that the Report expressly addresses proposed development, design objectives and purposes, and then only to the extent that there has been no material alteration to or variation from any of the said descriptions provided to Thurber, unless Thurber is specifically requested by the Client to review and revise the Report in light of such alteration or variation.

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- b) Reliance on Provided Information: The evaluation and conclusions contained in the Report have been prepared on the basis of conditions in evidence at the time of site inspections and on the basis of information provided to Thurber. Thurber has relied in good faith upon representations, information and instructions provided by the Client and others concerning the site. Accordingly, Thurber does not accept responsibility for any deficiency, misstatement or inaccuracy contained in the Report as a result of misstatements, omissions, misrepresentations, or fraudulent acts of the Client or other persons providing information relied on by Thurber. Thurber is entitled to rely on such representations, information and instructions and is not required to carry out investigations to determine the truth or accuracy of such representations, information and instructions.
- c) Design Services: The Report may form part of design and construction documents for information purposes even though it may have been issued prior to final design being completed. Thurber should be retained to review final design, project plans and related documents prior to construction to confirm that they are consistent with the intent of the Report. Any differences that may exist between the Report's recommendations and the final design detailed in the contract documents should be reported to Thurber immediately so that Thurber can address potential conflicts.
- d) Construction Services: During construction Thurber should be retained to provide field reviews. Field reviews consist of performing sufficient and timely observations of encountered conditions in order to confirm and document that the site conditions do not materially differ from those interpreted conditions considered in the preparation of the report. Adequate field reviews are necessary for Thurber to provide letters of assurance, in accordance with the requirements of many regulatory authorities.

6. RELEASE OF POLLUTANTS OR HAZARDOUS SUBSTANCES

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BASE PLAN 37507-C FROM ALBERTA TRANSPORTATION
Alberta
NORTH CENTRAL REGION (ATHABASCA AND FORT MCMURRAY DISTRICTS) 2024 GEOHAZARD ASSESSMENT NC097: HWY 686 (PARSONS ROAD OVERPASS) / HWY 63 SITE INSPECTION PLAN
FIGURE 1
DRAWN BY ML DESIGNED BY JGP
n DATE
FILE NO. 32122 THURBER ENGINEERING LTD.





Photo No. 1 – Looking south at the crack developed across the westbound lanes towards the median. The main crack is 20 to 40 mm wide x 10 to 40 mm deep. The cracks are across both traffic lane directions and have formed between the approach slab and the pavement, about 6 m west of the west abutment fingerplate; a new ACP patch was noted in 2024.



Photo No. 2 - Looking east at east bound lane. Cracks up to 60 mm wide and 90 mm deep





Photo No. 3 – Looking south at east bound lane. Cracks up to 60 mm wide and 90 mm deep



Photo No. 4 – A Flexible filler placed in 2024 to seal the 50 mm wide separation gap between the northwest wing wall and the drain trough. However, up to 300 mm deep gap was noted below the drain trough in response to fill settlement





Photo No. 5a – (Taken in Spring of 2023) Looking south at head slope movement (300 mm vertical drop x 300 mm lateral shift towards east); Void under abutment seat ranges from 0.8 m to 2.7 m.



Photo No. 5b – (Taken in Spring of 2024) Void under the abutment seat shown in photo 5a was filled with grout; However, ground appears to have dropped by 20 mm and displaced laterally by 10 mm at this location





Photo No. 6 – Bridge bearings appear to have maxed out.



Photo 7 – South drain trough. The gap between the drain trough and wingwall was sealed with a flexible filler.





Photo 8 – Water ponding and rutting at the toe of the bridge west headslope