# ALBERTA TRANSPORTATION GEOHAZARD ASSESSMENT PROGRAM NORTH CENTRAL REGION – ATHABASCA & FORT MCMURRAY DISTRICTS 2022 SITE INSPECTION



| Site Number                   | Location             |  |  | Name                      |            | Hwy          | km                  |  |
|-------------------------------|----------------------|--|--|---------------------------|------------|--------------|---------------------|--|
| NC091-1                       |                      | o 6 Km south of  |  | HWY 63-02 BACKSLOPE       |            |              | 39.27 and           |  |
| NC091-2                       | Wanderin             | g Riv  | er   | SLUMPS                    |            | 63:02        | 40.28               |  |
| Legal Description             |                      |  | UTM Co-c   | ordinates (NAD 8          | 3)         |              |                     |  |
| NC091-1: 6 km south of Wander |                      |  | ig River   | NC091-1 N6113146.92 E4056 |            | E405688.     | 87                  |  |
| NC091-2: 5 km south of Wan    |                      | nderin   | ig River   | NC091-2 N6112146.20       |            | E405659.     | E405659.10          |  |
|                               |                      |  | ·  |                           |            |              |                     |  |
|                               |                      | Date   |  | PF                        | CF         | Tot          |                     |  |
| Previous Inspec               | Previous Inspection: |  | ne 24, 2020  | 11                        | 3          | · ·          | 33 (NC091-1)        |  |
|                               |                      |  |  | 11                        | 3          | 33 NC091-2)  |                     |  |
| Current Inspection:           |                      | June 07, 2022  |  | 13                        | 3          |              | 39 (NC091-1)        |  |
| ourrent inspection.           |                      |  |  | 11                        | 3          | 33 (NC091-2) |                     |  |
| Road AADT:                    | Road AADT:           |  | 3,970  |                           | Year:      | 2021         |                     |  |
| Inspected By:                 |                      | Tarek Abdelaziz, José Pineda (Thurber)<br>Arthur Kavulok, Amy Driessen, Rishi Adhikari (TRANS) |  |                           |            |              |                     |  |
| Report Attachments:           |                      | <b>₽</b> F   | Photographs Plans  |                           |            |              | C Maintenance Items |  |
| Primary Site Issue:           |                      |  | Active landslides toeing out in the highway east ditch, encroaching into private lands, but not impacting the highway<br><b>NC091-1:</b> The slide is 150 m wide (parallel to the highway), 26 m long  |                           |            |              |                     |  |
| Dimensions:<br>Maintenance:   |                      |  | <ul> <li>(perpendicular to the highway), and the backslope is 8 m high (from the crest to the toe) and inclined at 3H:1V.</li> <li>NC091-2: The slide is 110 m wide (parallel to the highway), 35 m long (perpendicular to the highway), and the backslope is 7 m high (from the crest to the toe), and inclined at 3H:1V</li> <li>None</li> </ul> |                           |            |              |                     |  |
| Observations:                 |                      |  |  |                           | escription |              | Worse?              |  |
| Observations:                 |                      |  | NC001-1-11   | WUISe :                   |            |              |                     |  |
| Slope Movement                |                      |  | NC091-1: U<br>farmer's field<br>the tension<br>mm to<br>700 mm wid-<br>and it is abou<br>NC091-2: 1<br>significantly<br>tension crac<br>the width<br>700 mm. Th<br>and it is parti   | 2                         |            |              |                     |  |
| ✓ Seepage                     |                      |  | <b>NC091-1 and NC091-2:</b> wet landslide mass; ponding water within few locations of the landslide mass; toe roll partially blocking water flow along the ditch; catch water ditch near the crest of both slides was impacted by the landslide movement and water from the catch water ditch saturated the landslides.                            |                           |            |              | V                   |  |

| ✓ Other | <b>NC091-1:</b> A severe erosion gully developed within the farmer's field; the gully is about 12 m long x 12 m wide with 1.3 m drop at the deepest location.<br><b>NC091-2:</b> Severe erosion around the half pipe and the riprap apron; erosion extended to the south of the catch water ditch into private land; half pipe got completely separated from culvert near the top of the slope; landslide mass became more vegetated than observed in 2020. | V |
|---------|---|---|
|---------|---|---|

## Instrumentation (1SIs and 4PNs):

**NC091-1:** SI18-1 was installed near the toe roll, and SI18-2 near the crest of the landslide. SI18-2 was sheared off at about 3.0 m depth below ground surface a few months after installation. SI18-1 has a current rate of movement of 2 mm/yr at 1.4 m depth and the movement rate increased by 6.1 mm/yr since the previous readings in the spring of 2021.

Groundwater levels ranged between 8.2 m in PN18-2B to 9.0 m in PN18-1. The water levels did not change significantly since the previous readings. PN18-2A was damaged during the 2022 inspection, but the highest recorded groundwater level in PN18-2A was 1.1 m below ground surface in the spring of 2018.

**NC091-2:** SI18-3 was installed near the toe roll, and SI18-4 near the crest of the landslide. SI18-4 was sheared off at about 3.4 m below the top of casing a few months after installation. SI18-3 was damaged, likely by a lawnmower, and has not been read since the spring of 2019.

Groundwater levels ranged between 1.7 m in PN18-4A (near surface clay) to 12.7 m in PN18-4B (in the clay till). The water levels increased since the previous readings in the spring of 2021 by 0.1 m and 0.4 m in PN18-4B, and PN18-4A, respectively. PN18-3 was damaged during the 2022 inspection but the highest recorded groundwater level in PN18-3 was 5.1 m below ground surface in the fall of 2018.

## **Assessment** (Refer to attached Figures):

The backslope landslides continued to be active, but NC91-1 appears to be moving at a higher rate than NC91-2 based on the site observations. Therefore, the Probability of Failure for the NC91-1 site was increased from 11 to 13.

The landslides are shallow and do not appear to extend below the highway ditch bottom. The soil within the backslopes consist of 3 to 4 m of soft to firm high plastic clay with occasional sand/silt pockets underlain by sand and clay till. A sand layer was however noted in the test hole near the crest of he NC91-1 site. The slip surface is within the high plastic clay at both sites. Piezometer readings indicate that groundwater levels in the clay are much higher than the underlying strata. It is likely that the slumps have been triggered due to ground water seepage (likely from the catch water ditch) into the clay though the sand/silt pockets resulting in softening of the clay and hence loss of its strength. The failure of half pipe at NC92-2 may have aggravated the situation. In addition, the backslopes appear to be relatively steep, when considering the high plasticity of the clay and the heights of the slope, and this may have been another contributing factor to the observed failures.

It is anticipated that both slumps will continue to be active and retrogress to cause further loss of private lands. Future prolonged heavy rainfall events are anticipated to increase groundwater levels in the landslides resulting in accelerated movements. In addition, the existing catch water ditches near the crest of both landslides have been impacted by the landslides and water is being discharged into both landslide masses. Surface water discharge into the landslide mass at both sites will continue to elevate groundwater levels in the slopes.

The presence of open wide cracks and erosion gullies within the private properties is a safety concern.

The landslide debris is partially blocking the highway ditch at both locations and hence impeding surface drainage in the highway ditch. This may result in elevated groundwater levels in the highway embankment and potential instabilities in the future.

### **Recommendations:**

It is recommended to visit these sites again in 2024.

# Short-Term

The owners of the land parcels located near the top of the backslope at both slump locations should be advised of the risk that exists at these locations.

The local MCI should consider the following:

(a) undertake slight grading of the highway ditch at the slump locations, as needed, to promote surface drainage. Excavated material from the ditch should be pushed back against the toe of the slope. Excessive removal of landslide debris from the toe of the slope could result in accelerated movement,

(b) seal open cracks in the slope surface to reduce surface water infiltration into the slide mass. A small track mounted equipment could be used to smoothen the slope surface and fill in any dips without causing significant changes in grade,

(c) place a snow fence around areas impacted by the landslide within the private lands or backfill these areas to eliminate existing hazard. However, this can only take place after consultation with the landowner(s).

# Long-Term

There are two potential general approaches that could be considered for the repair of these sites:

- 1. Excavate and replace the slide material with imported low to medium plastic clay and reconstruct the slope at the original inclination (3H:1V). In this option, a gravel drainage blanket should be included along the back and at the base of the excavation to promote drainage. At least two subdrain pipes will need to be included along the base of the excavation within the drainage blanket to direct the flow into a controlled manner into the ditch; or
- 2. Excavate and reconstruct the backslope to 4H:1V or flatter. In this option, excavated materials will need to be reworked (moisture conditioned) before being recompacted, if the material is deemed suitable. A drainage blanket and closely spaced subdrains will need to be included in the reconstructed slopes to promote drainage. Acquisition of additional ROW will be required if it is decided to pursue this option.

For any of the above options, the subdrain pipes will need to daylight into the highway ditch. Riprap protection of the ditch will be needed within the repaired area to prevent future erosion issues.

At both sites, the catch water ditch will need to be reconstructed using low to medium plastic clay, realigned to be a few meters away from the top of the slope in the vicinity of the landslides, and lined with an impervious barrier to prevent further erosion and saturation of the slopes. At NC091-2, it is possible to re-grade the catch water ditch to drain towards a centerline culvert located south of the site at approximate km 40.090. During construction, the catch water ditch flow will need to be temporarily diverted away from the slope repair area.

The estimated cost of repairing each site would range from \$500K to \$700K excluding engineering.

# Closure:

It is a condition of this letter report that Thurber's performance of its professional services will be subject to the attached Statement of Limitations and Conditions.

Yours very truly, Thurber Engineering Ltd. Tarek Abdelaziz, Ph. D, P.Eng. Principal | Senior Geotechnical Engineer

José Pineda, M.Eng., P.Eng. Associate | Geotechnical Engineer



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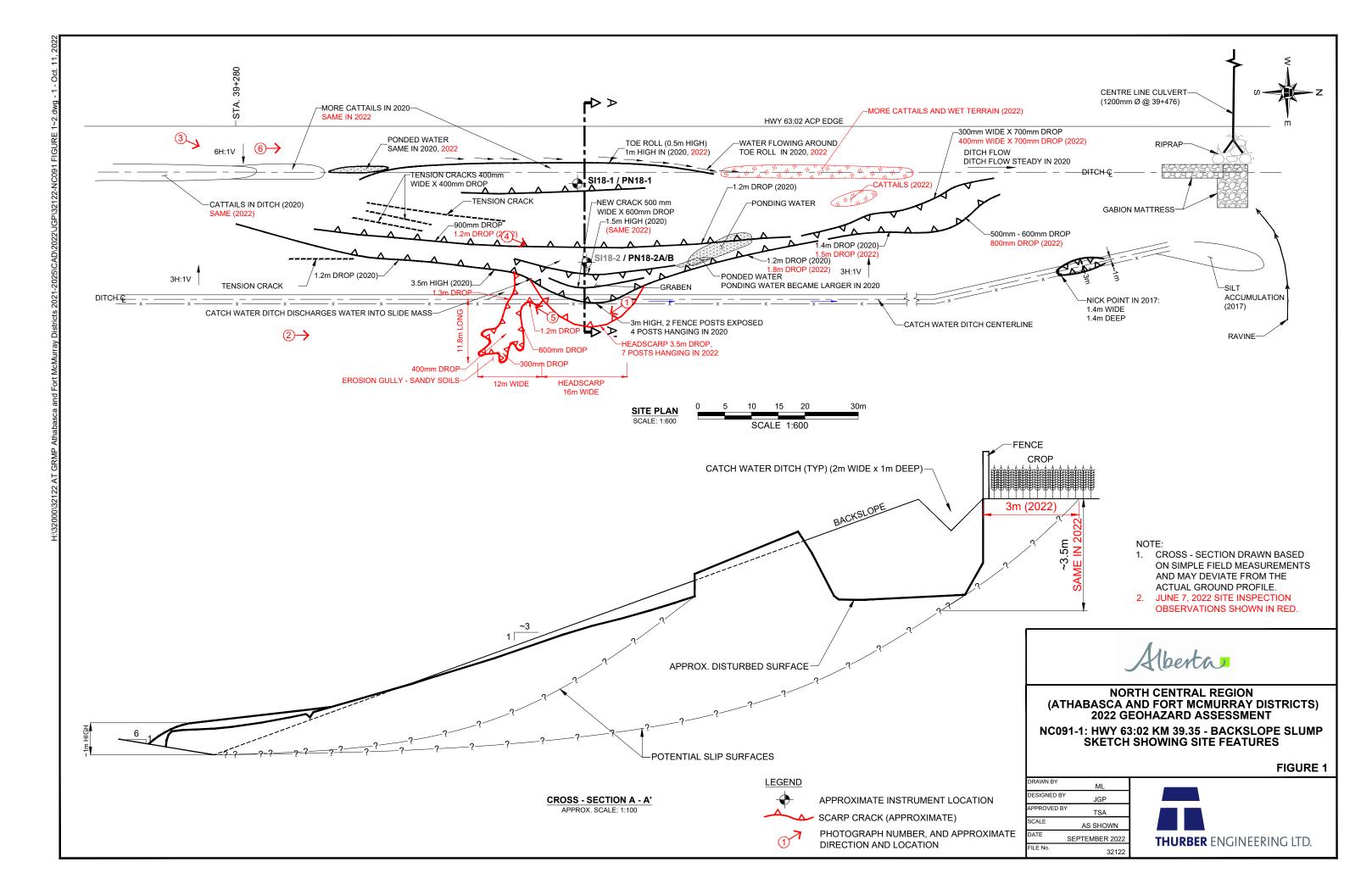
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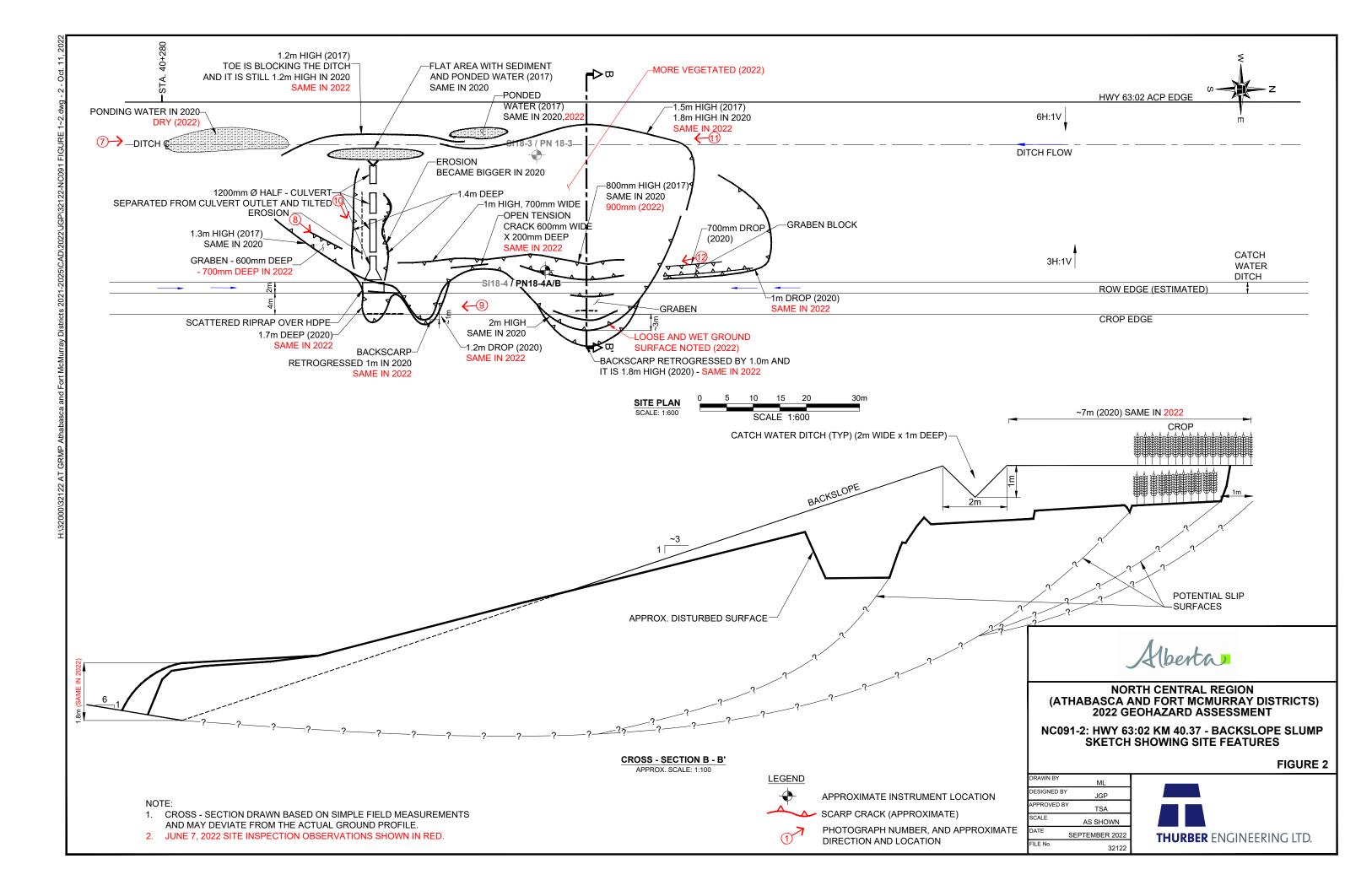






Photo No. 1- NC091-1: Looking southeast where the landslide cuts through catch water ditch; catch water ditch discharges water into the landslide mass



Photo No. 2- NC091-1: Looking north at a 12 m long erosion gully developed within the farmer's field; note the presence of sandy soils within the exposed surfaces of the gully walls





Photo No. 3- NC091-1: Looking northeast at the landslide mass; note the presence of multiple tension cracks in the slope and cattails in the highway ditch



Photo No.4 - NC091-1: Looking northeast at the north flank of landslide;3.5 m deep cracks and seven barbed wire posts hanging in 2022





Photo No. 5 - NC091-1: Looking southwest at the head scarp crack and the erosion gully developed within the farmer's field



Photo No. 6 – NC091-1: Looking north at a distinct toe roll in the ditch





Photo No. 7 – NC091-2: Looking north at the landslide mass; note the presence of a distinct toe roll in the ditch



Photo No. 8– NC091-2: Looking northeast at the southern flank of the landslide mass; note the presence of multiple tension cracks within the backslope





Photo No. 9 – NC091-2: Looking south at scarp crack developed within the crest of the backslope



Photo No. 10 – NC091-2: Looking northeast at a scarp crack through the riprap apron and into the adjacent field (south scarp)





Photo No. 11 – NC091-2: Looking south at landslide features; note the well-defined toe roll at the ditch and the presence of multiple tension cracks within the backslope; landslide appears to be more vegetated than in 2020



Photo No. 12 - NC091-2: Looking south at the northern flank of the landslide