ALBERTA TRANSPORTATION GEOHAZARD ASSESSMENT PROGRAM NORTH CENTRAL REGION – ATHABASCA & FORT MCMURRAY DISTRICTS 2022 SITE INSPECTION



Site Number	Loc	cation		Name		Hwy	km	
NC087		75 km north of the FISCHER TRAIL SLIDE 63:02		20.75				
Legal Description				UTM Co-or	dinates (NAD 83			
SE-22-69-17-W4M				12 N	6094104.70	E 4	04166.89	
			Date	PF	CF	Т	otal	
Previous Inspection	revious Inspection:		June 24, 2021		4	56 (Highway 63)		
Current Inspection:	urrent Inspection:		June 7, 2022		4	56 (Highway 63)		
Road AADT:	oad AADT:		3,850		Year:	2021		
Inspected By:			ineda, Tarek Ab Kavulok, Rishi A			ber) Driessen (Alberta Transportation)		
Report Attachments	eport Attachments:		Photographs		✓ Plans		□ Maintenance Items	
Primary Site Issue		 Upper landslide block: Active slide movement causing severe distress for about 140 m along the Fischer trail surface and affecting Hwy 63 southbound lanes west side slope. Lower landslide block: Active slide movement causing severe distress for about 85 m along Fischer trail surface. 						
Dimensions:		Upper landslide block: About 140 m wide along the trail alignment and 120 m long perpendicular to the trail alignment.Lower landslide block: About 90 m wide along the trail alignment and 95 m long perpendicular to the trail alignment.						
Site History/Maintenance:		Fischer trail is a gravel surfaced road located on the west side of the HWY 63:02 southbound lane embankment. Based on discussions with AT and WSP, it is understood that Fischer Trail is a private road that was upgraded in 2014 during the construction of the highway twinning project at this location as part of land negotiations. Prior to construction, the subject area was low-lying and covered with shrubs and trees. During construction, about 1 m to 1.5 m of peat was removed from below the trail alignment to expose the firm clay foundation. As per the information provided by WSP, it is understood that up to 3 m of clay fill was placed on the exposed native clay to establish the design profile of the trail. However, shortly after the fill was placed, tension cracks were noticed along the trail surface and near the toe of the highway embankment side slope. The movement has also resulted in the tilting of one of the power poles. Survey monitoring was conducted after the cracking was observed and a vertical drop of 50 to 70 cm was noted shortly after monitoring began. During construction, an attempt to stabilize the slope was made by flattening the side slope of Fischer trail and re-grading the road. Thurber was called out to the site during construction in September 2014 and May 2015 and preliminary assessment letters were submitted to WSP. In 2015, the survey monitoring program						

	conducted by WSP indicated a reduction in the movement rates and hence a decision was made to seal up open cracks on the highway side slope and to get the Fortis Alberta to straighten the affected power pole. Based on information provided by AT in early 2017, it is understood that the Fischer Trail lease was recently extended until December 15, 2025, and the road authority was transferred over to the County of Athabasca November 18, 2015. AT resurfaced the trail with gravel in late 2016.						
Observations:	Description	Worse?					
Pavement Distress	Longitudinal and transverse cracks on the HWY (SBL) 40 to 50 mm wide no drop; no noticeable dips on HWY 63:02 paved surface						
Slope Movement	Tension crack within 6.5 m from the edge of the highway; open head scarp cracks within the upper and lower landslide blocks (100 to 700 mm wide, and 100 mm to 1 m drop); leaning/tilting trees between the west edge of the trail and the pronounced toe roll area						
Based on 2021 Inspection on the Trail							
Erosion	the erosion gully within the trail east ditch (10 m long x 2 to 3 m wide x 0.8 m deep) and at the 800 mm diameter culvert inlet (4.5 m long x 3.5 m wide x 1.5 m deep)						
I Seepage	Fisher trail surface is wet and standing water was noted in the trail surface and the east ditch; previously noted water ponding in the highway east ditch between culverts C2 and C3 located to the south of the landslide area was dry. Water is partially flowing under culvert C3 inlet.						
✓ Bridge/Culvert Distress	Severe sinkholes and subsidence along Fischer trail; The existing 800 mm CSP culvert, installed during construction below the trail had been separated resulting in the formation of multiple sinkholes that have converged into a large sinkhole (6 m in diameter and 1.5 m deep);						
✓ Other	La Biche River outside bend of the meander is located 90 m and 125 m to the west of the western edge of the trail and highway, respectively. Fence posts have moved approximately 1 m toward the river. Power poles are tilting within the slide area by 2 degrees.						

Instrumentation Readings (3 PN and 2 SP piezometers):

Between the spring and the fall of 2018: SI17-1, SI17-2 and SI17-3, installed near the edge of the trail, were sheared off at depths varying between 5.6 m and 8.1 m below the trail surface; SI17-5, installed between the fence and the highway was damaged at 1.3 m below ground surface. SI17-1, SI17-2, SI17-3 and SI17-4 moved at maximum rates ranging between 55 and 160 mm per year.

Groundwater levels in the pneumatic piezometers ranged between 1.0 m below ground surface to 0.2 m above ground surface (artesian). The groundwater level in standpipe piezometers is within 0.7 m below ground surface.

Assessment (Refer to attached Figures):

The site condition did not change significantly since the 2021 site inspection.

Based on the above site observations, and LiDAR information, the distress observed along Fischer trail and the side slope of the highway SBLs reflects an actively moving deep-seated landslide. The depth of movement ranges from 5.6 to 8.1 m below the trail surface. The landslide continues to cause severe distress of the trail surface and is retrogressing to the highway surface.

It is suspected that the low-lying area of the original trail alignment was located within the crest of an ancient landslide, toeing into the outside bend of the La Biche River. Placement of grading fill to construct the trail could have resulted in (a) re-activation of the ancient landslide, and (b) obstruction of natural drainage pattern, resulting in elevated ground water levels in the slope area.

The surface water in the trail ditch flows below the separated 800 mm diameter culvert, resulting in the saturation and washout of trail fill and subgrade and recharging of the landslide mass. It is likely that the uncontrolled discharge of surface water below the trail will result in the formation of additional sinkholes and potentially complete failure of the trail.

The trail surface is in a very poor condition, and it constitutes a safety hazard to the trail users.

The landslide continues to be active, and this will eventually result in further failure of the trail surface, the retrogression of the landslide into the highway lanes due to continued loss of support at the toe of the slope, and potential damages to the fence line, Telus cable and the overhead power lines.

Recommendations:

This site should be visited again in the spring of 2023.

In the short term, we recommended the following:

- AT should contact the County, the trail owner, and utility companies to let them know about existing hazard(s).
- The local MCI should periodically monitor the head scarp crack for further opening or drop and measure the distance between the head scarp crack and the edge of the highway.
- Clear sedimentation and regrade the ground surface near culvert C1 outlet; inspect and maintain culverts C2 and C3 as needed to prevent further ponding of water in the highway west ditch and water flow under C3.

It is understood that AT has no obligation to maintain the trail. Hence, the long-term measure may include the construction of a pile wall between the head scarp crack and the west edge of the highway to shelter the highway from potential retrogression of the head scarp crack into the highway surface. The ballpark cost of this option, excluding engineering, would be in the range of \$850,000 for a steel pile wall and \$2.0 Million for a tangent cast-in-place cantilever pile wall. It should be noted that this option will not address the impact of future movements downslope of the wall on existing trail and utility lines within the landslide mass.

Closure:

It is a condition of this letter report that Thurber's performance of its professional services will be subject to the attached Statement of Limitations and Conditions.

Yours very truly, Thurber Engineering Ltd. Tarek Abdelaziz, Ph.D., P.Eng. Principal | Senior Geotechnical Engineer

José Pineda, M.Eng., P.Eng. Senior Geotechnical Engineer



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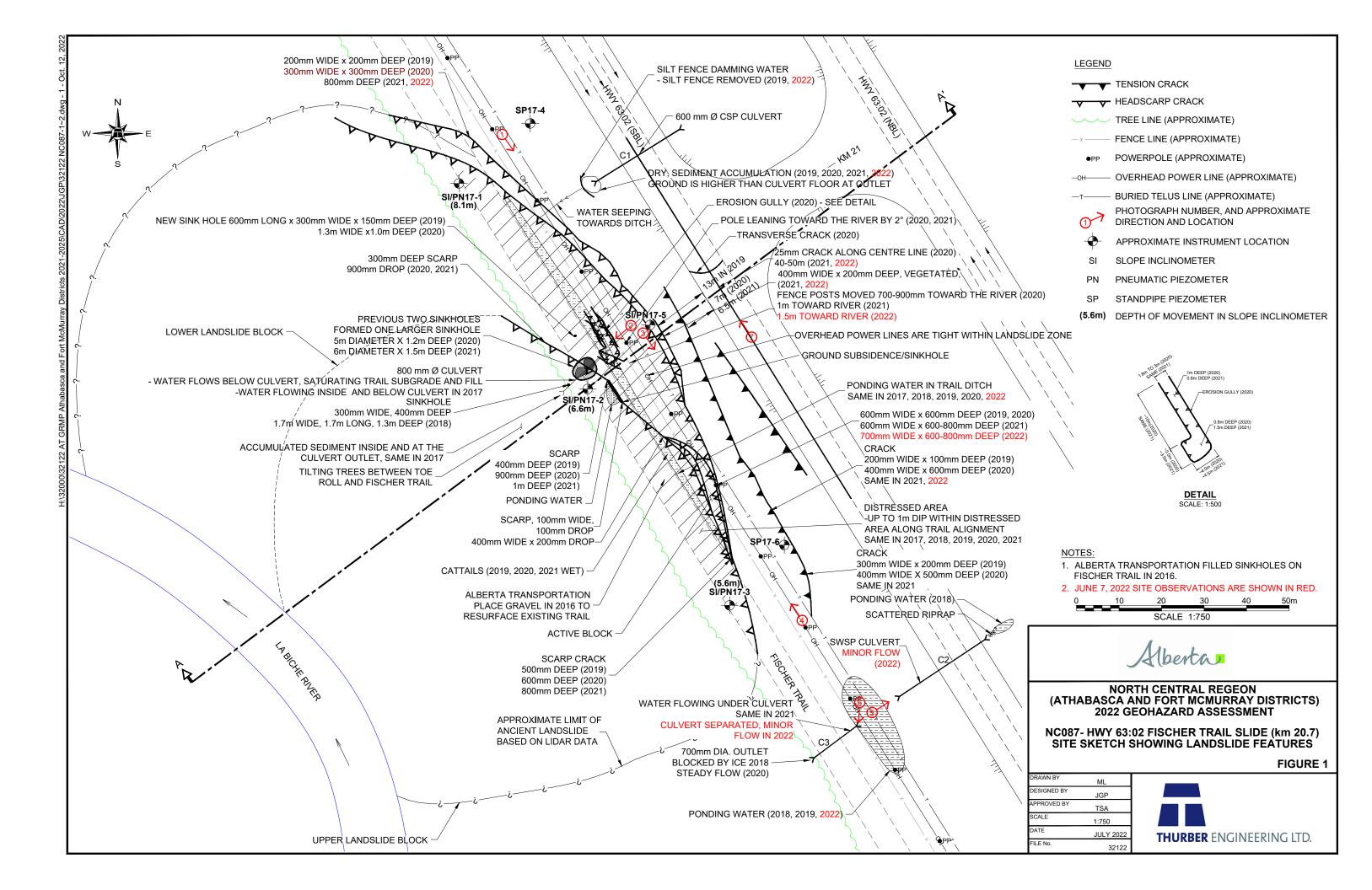
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- c) Design Services: The Report may form part of design and construction documents for information purposes even though it may have been issued prior to final design being completed. Thurber should be retained to review final design, project plans and related documents prior to construction to confirm that they are consistent with the intent of the Report. Any differences that may exist between the Report's recommendations and the final design detailed in the contract documents should be reported to Thurber immediately so that Thurber can address potential conflicts.
- d) Construction Services: During construction Thurber should be retained to provide field reviews. Field reviews consist of performing sufficient and timely observations of encountered conditions in order to confirm and document that the site conditions do not materially differ from those interpreted conditions considered in the preparation of the report. Adequate field reviews are necessary for Thurber to provide letters of assurance, in accordance with the requirements of many regulatory authorities.

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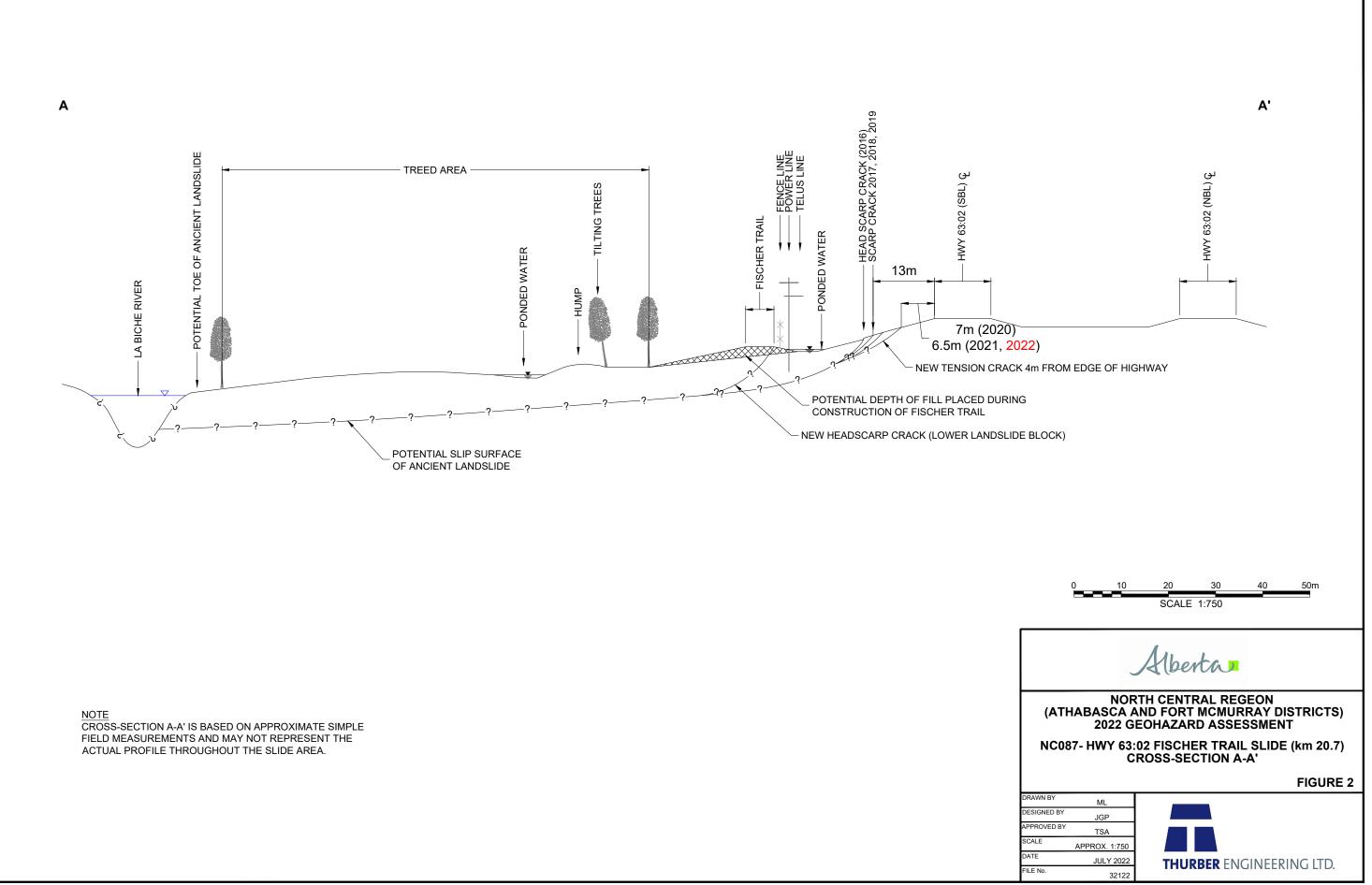






Photo No.1 – Head scarp crack of upper landslide block (Looking South)



Photo No.2 – Sinkhole above the 800 mm diameter culvert; looking at the culvert inlet





Photo No.3 – Looking south at the southern flank of the landslide (700 mm wide, 600-800 mm deep); water ponding along the ditch between the trail and the fence (note cattails in this area)



Photo No.4 –Looking north at the southern flank of upper and lower landslide blocks; note standing water within the flank and lateral shifting of existing fence; landslides are well vegetated





Photo No.5 – Outlet of SWSP culvert C2; minor flow observed in 2022



Photo No.6 - 700 mm diameter CSP culvert C3 inlet; culvert separated; minor flow noted in 2021





Photo No. 7 – Looking north at highway southbound lanes; landslide is not currently impacting the highway surface; head scarp crack is about 6.5 m away from the edge of pavement